



# Constructing and Testing a Low Permeability Barrier Using Weathered Mine Spoil

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# Presentation Outline

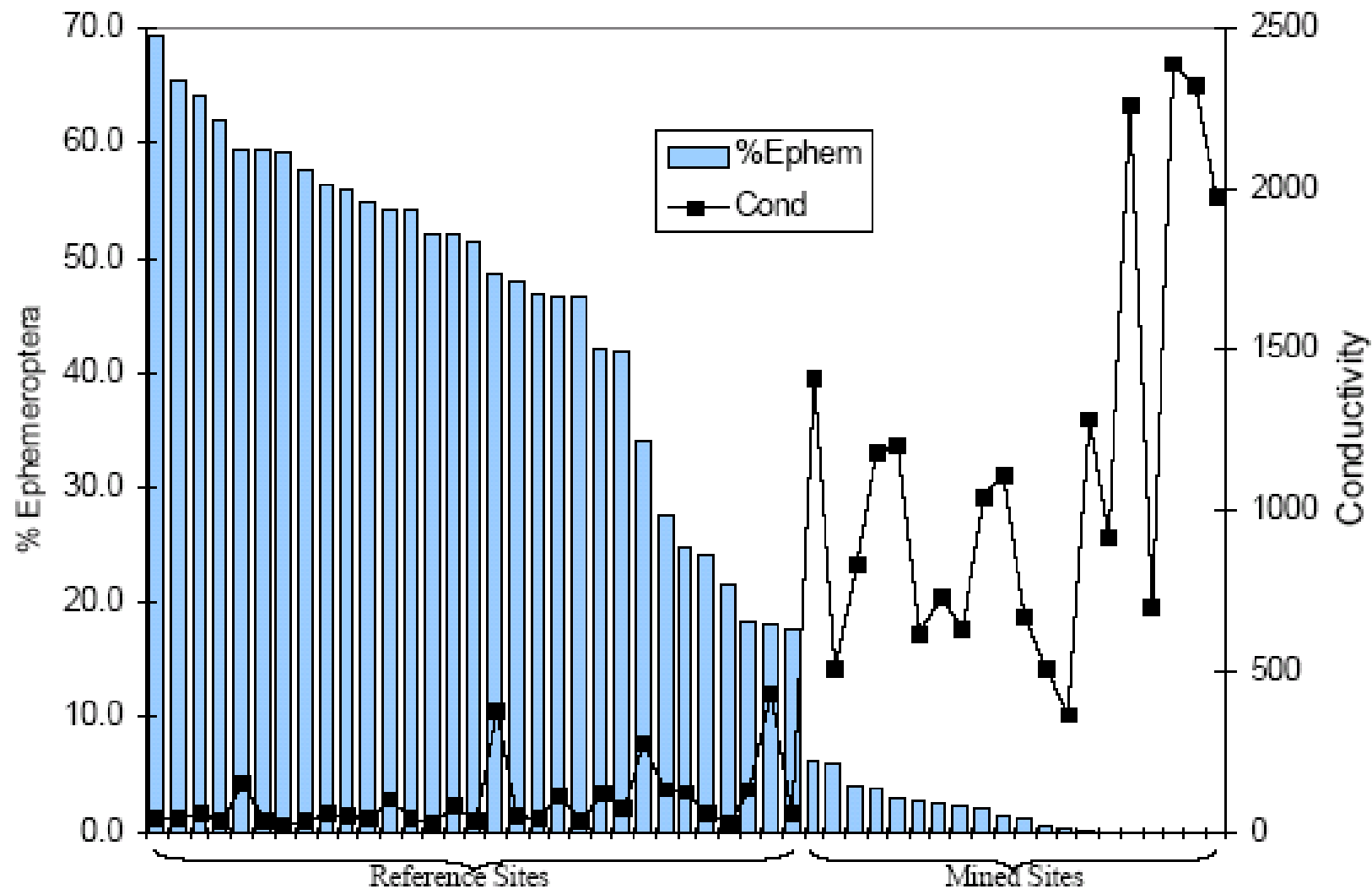
- Environmental challenges in Appalachia Coalfields
- Problematic strata identification and isolation
- Project objective
- Methodology
- Results
- Implications



# Environmental Challenges

- Mining process breaks apart rocks into smaller fragments creating larger surface areas that can interact with water
- Can lead to water quality impairments





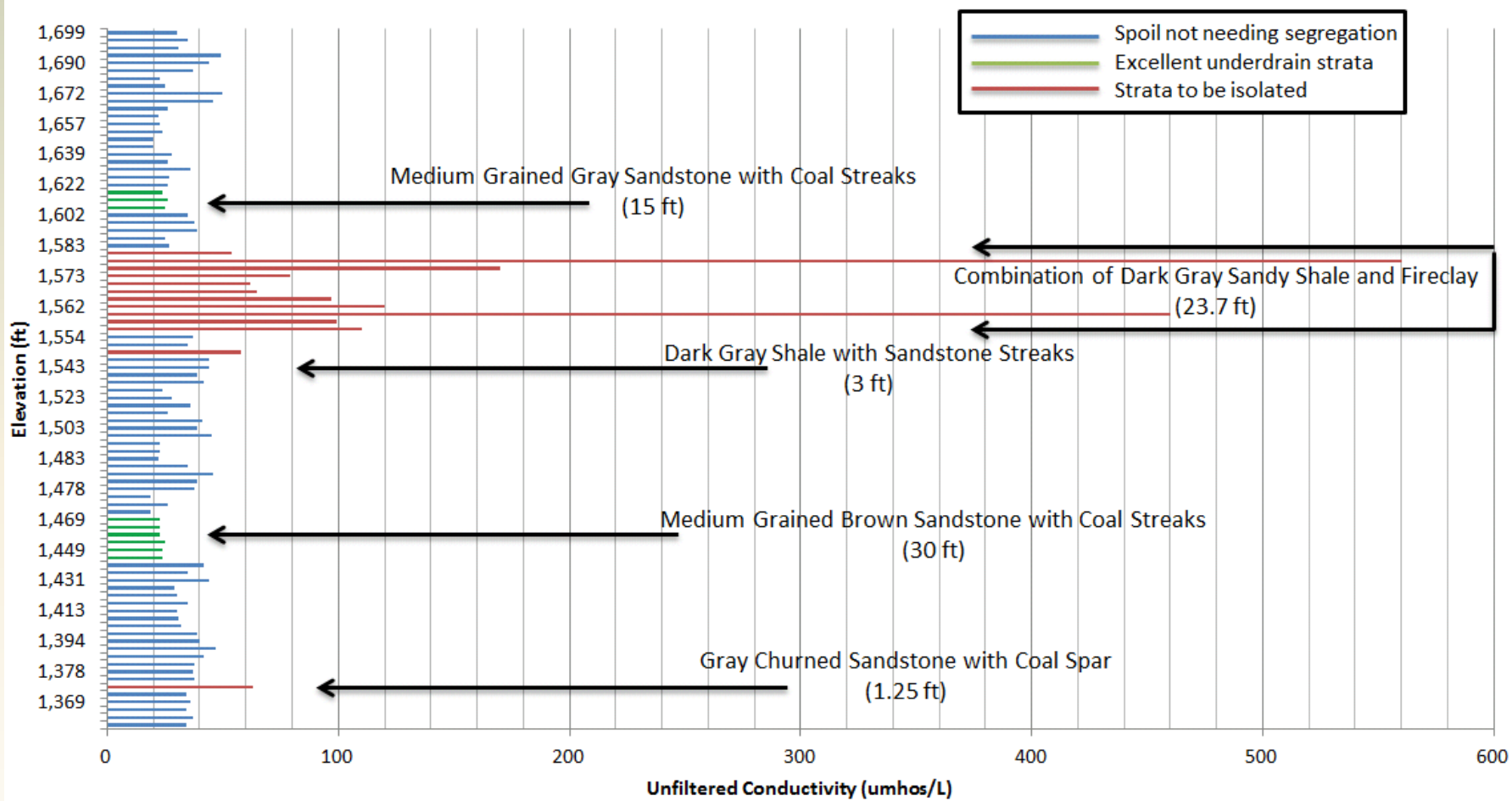
U.S. Environmental Protection Agency (USEPA)  
 Specific conductance (2011):  $300\text{-}500 \mu\text{S cm}^{-1}$



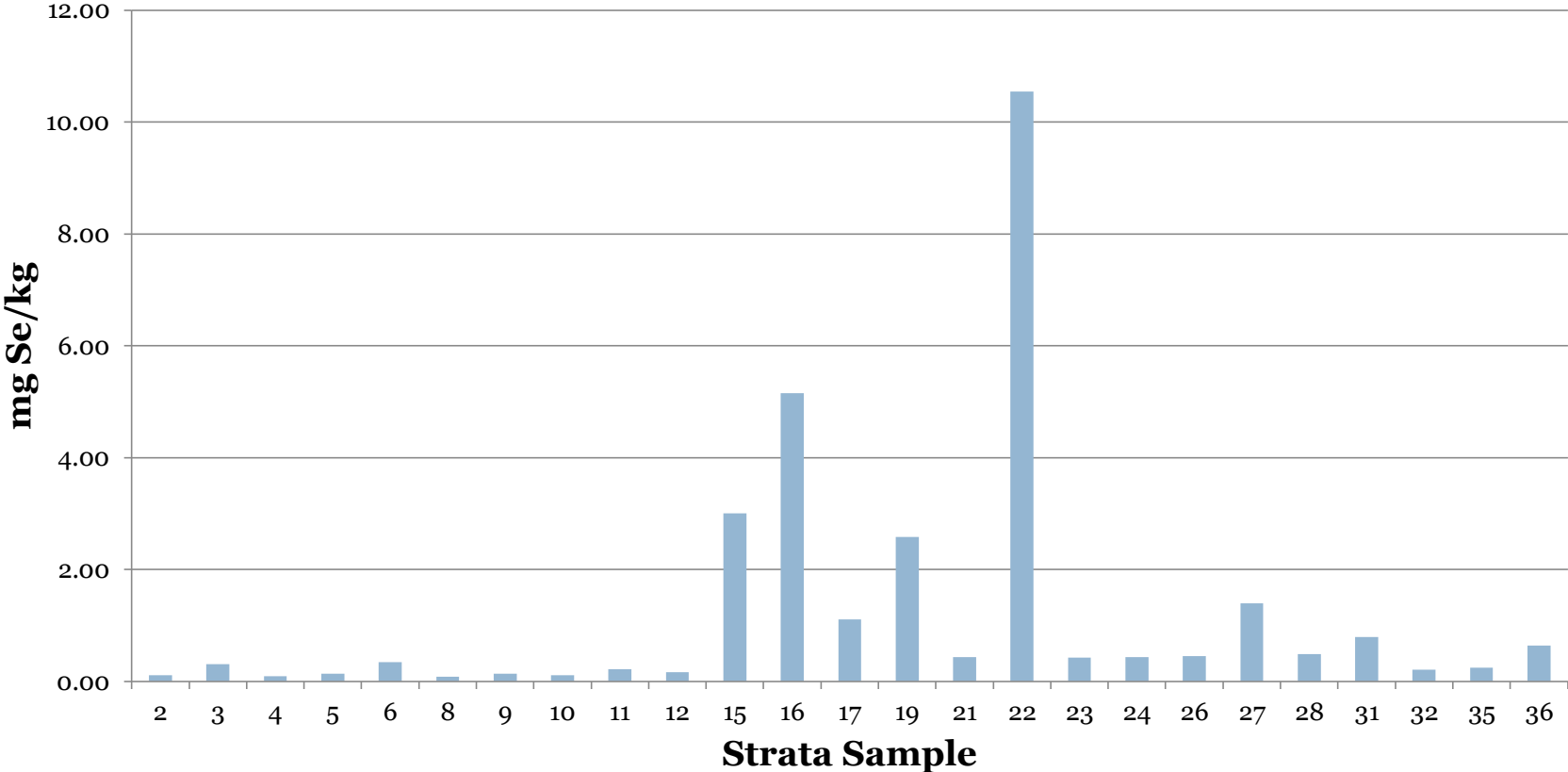
# Problematic Strata (Spoil) Identification

- Not all strata have same potential to generate high specific conductance and selenium levels





# Se Overburden Strata

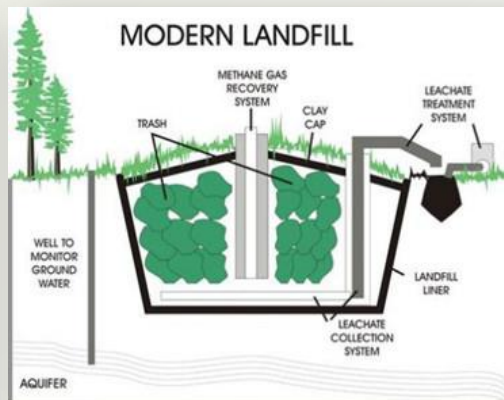


# Problematic Strata (Spoil) Isolation

- Prevent water from infiltrating into problematic spoil
- Spoil isolation one method traditionally used with acid producing materials (not most common)
- Literature plentiful for clay barriers
  - ▣ Municipal solid waste, hazardous waste, low-level nuclear waste



Source: asme.org



Source: Bounce Energy







**Weathered sandstone for use  
as spoil isolation barrier**

# Project Objectives

- Evaluate field saturated hydraulic conductivity levels on low permeability barrier constructed from weathered sandstones
- Compare field-based saturated hydraulic conductivity values to those obtained in the laboratory



# Study Site



# Low Permeable Barrier Construction

- Spoil dumped with CAT 777 and spread with CAT D9 dozer to nominal depth of 0.7 m
- Water incorporated as needed per da Rosa et al. (2013)
- One pass over entire layer with loaded CAT 777
- Continue layering technique until 3 m lift achieved (~6-7 layers per lift)



Source: cat.com



Source: cat.com



Source: cat.com

# Methods: Spoil Characterization

- Spoil collected in 19 L buckets
- UK Regulatory Services
  - ▣ Percent sand, silt and clay
  - ▣ USDA textural triangle (USDA-NRCS, 2012)
- Liquid limit, plastic limit, and plasticity index
- Shake test



# Methods: Laboratory Testing

- Standard proctor test (ASTM D698)
  - Maximum achievable level of compaction ( $\rho_{\max}$ ) for optimum moisture content (MC)
    - MC (gravimetric) ranged between 12-18%
- Saturated hydraulic conductivity ( $h_{\text{sat}}$ )
  - Rigid wall double-ring permeameter



# Methods: Field Testing

- Two double-square infiltrometers
  - Outer: 1 m x 1 m
  - Inner: 0.5 m x 0.5 m
- Installed to depth of 0.5 m using Class 200 excavator



# Methods: Field Testing

- Filled inner and outer boxes with water
  - ▣ Two holes used to fill inner box, later capped
  - ▣ 1 m vertical pipe to increase hydraulic head and measure infiltration
- Allowed spoil to saturate for 1 month
- Measured hydraulic gradient for 5-6 hours, 15-min intervals (until steady state achieved)





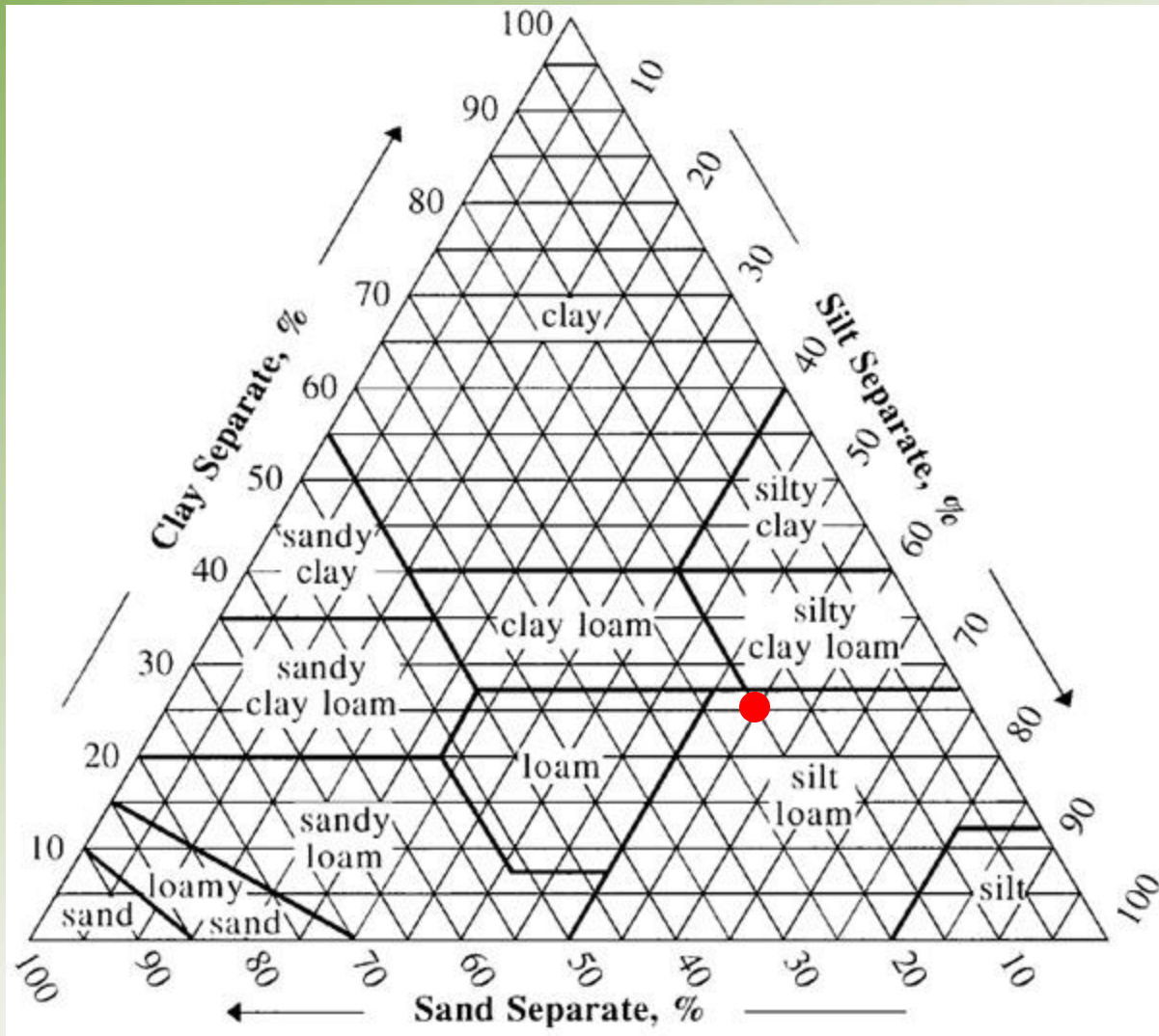
# Methods: Field Extracted Cores

- Four cores (0.7 m tall, 6.5 cm diameter)
- Compaction of spoil in core or below core
- Spoil could not be removed from core
  - ▣ Hydraulic conductivity measured in core tube in lab
  - ▣ Connected 5 m pipes to cores to expedite the process



# Results

- Spoil was silt loam (80.2% fines); ML in USCS classification; low  $EC_{25^{\circ}C}$ .
- Achieved average  $\rho_{max}$  of 2,100 kg m<sup>-3</sup> at MC of 15% and average  $h_{sat}$  of  $5.5 \times 10^{-8}$  at MC of 16%
- Results similar to those from da Rosa et al. (2013) for brown weathered sandstone
- Lab core results showed average  $h_{sat}$  of  $3.1 \times 10^{-9}$  for all cores (additional compaction occurred with sample collection)
- Achieved comparable  $h_{sat}$  in field with loaded truck as compared to lab with proctor



Sand:  $19.8 \pm 0.7$

Silt:  $54.1 \pm 0.3$

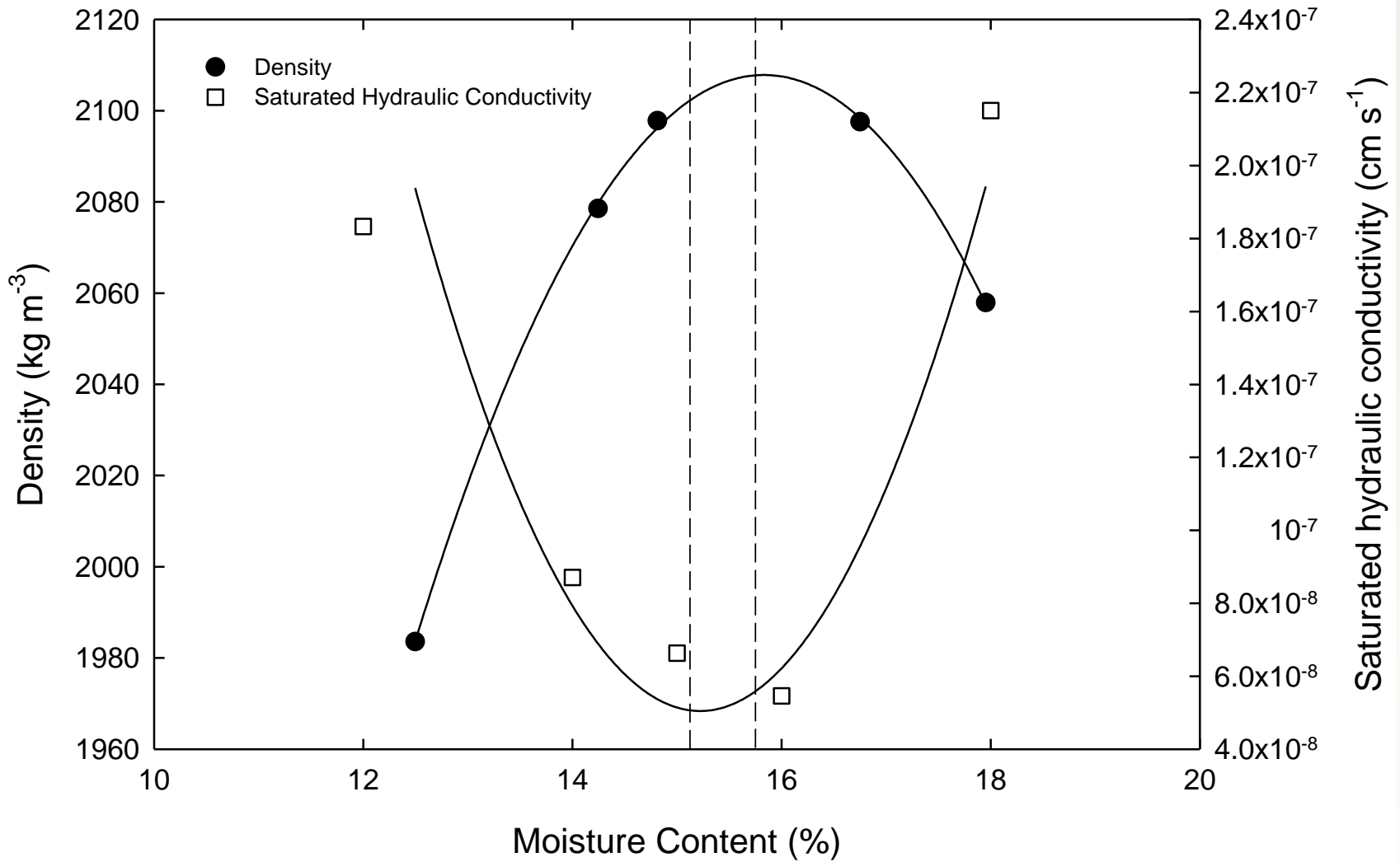
Clay:  $26.1 \pm 0.4$

Spoil Subsample	Liquid Limit (%)	Plastic Limit (%)	Plasticity Index (%)
1	26	25	1
2	25	25	0
3	25	25	0

Spoil Subsample	Specific Conductance ( $\mu\text{S cm}^{-1}$ )
1	42
2	41
3	38

# Results

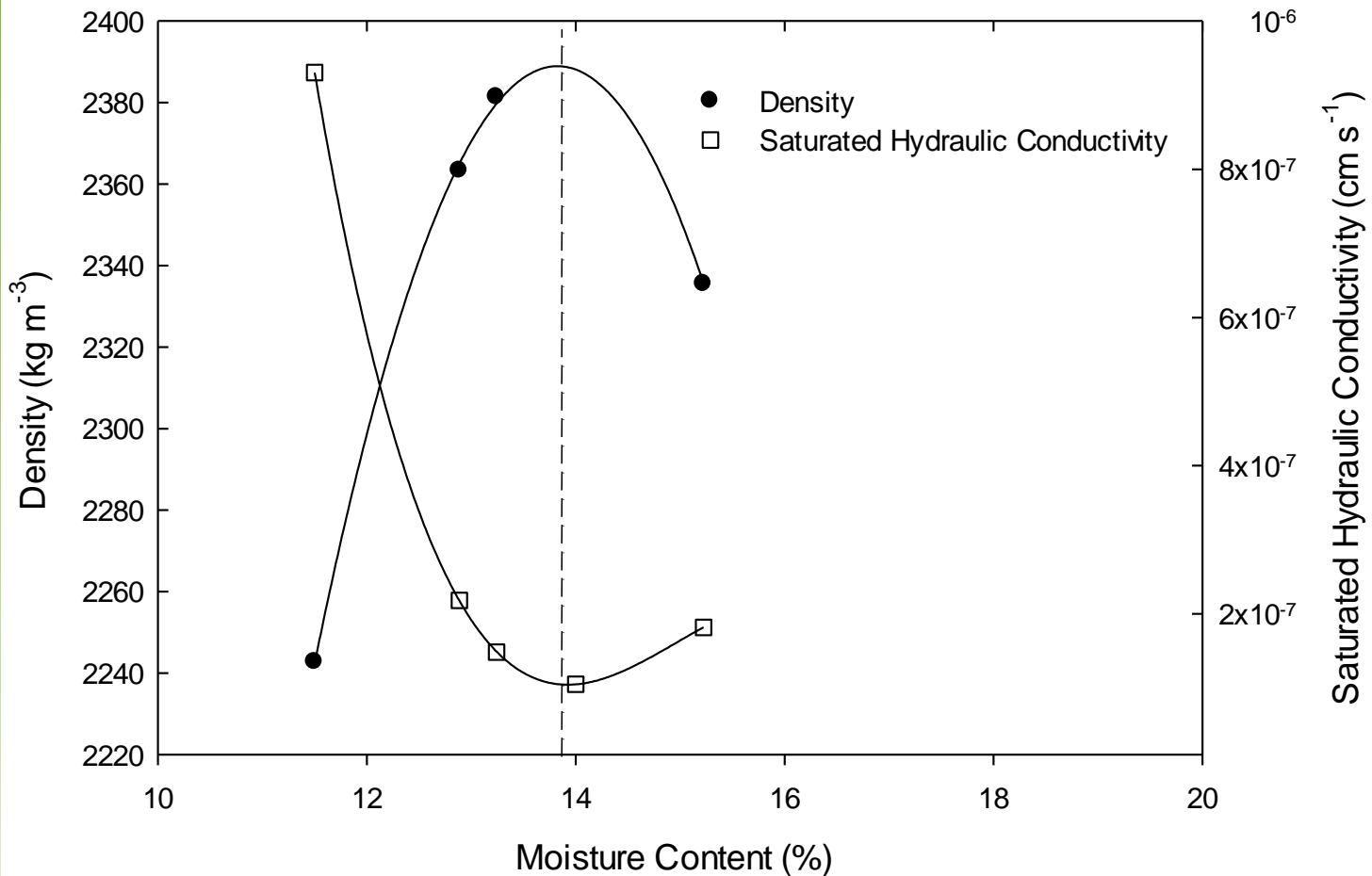
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$$\rho_{\max} = 2,100 \text{ kg m}^{-3} \text{ (MC=15\%)} \quad h_{\text{sat}} = 5.5 \times 10^{-8} \text{ (MC=16\%)}$$

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Brown weathered sandstone from same mine

$$\rho_{\max} = 2,400 \text{ kg m}^{-3} \text{ (MC=14\%)} \quad h_{\text{sat}} = 1 \times 10^{-7} \text{ (MC=14\%)}$$

52% sand, 34% silt, and 14% clay (48% fines)



# Results

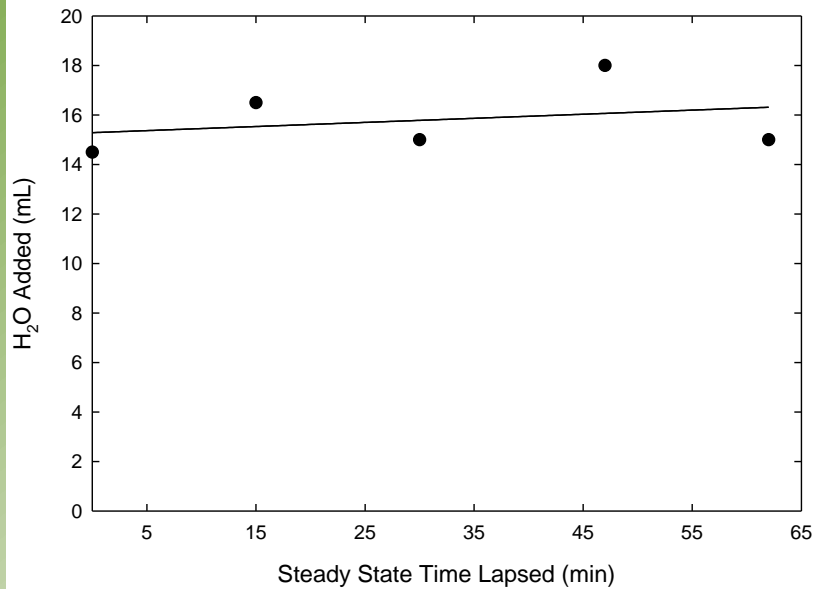
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Core ID	Average $h_{\text{sat}}$ (cm s <sup>-1</sup> )	% core filled
A	$2.1 \times 10^{-9}$	39
B	$2.0 \times 10^{-9}$	39
C	$6.8 \times 10^{-9}$	41
D	$1.4 \times 10^{-9}$	36

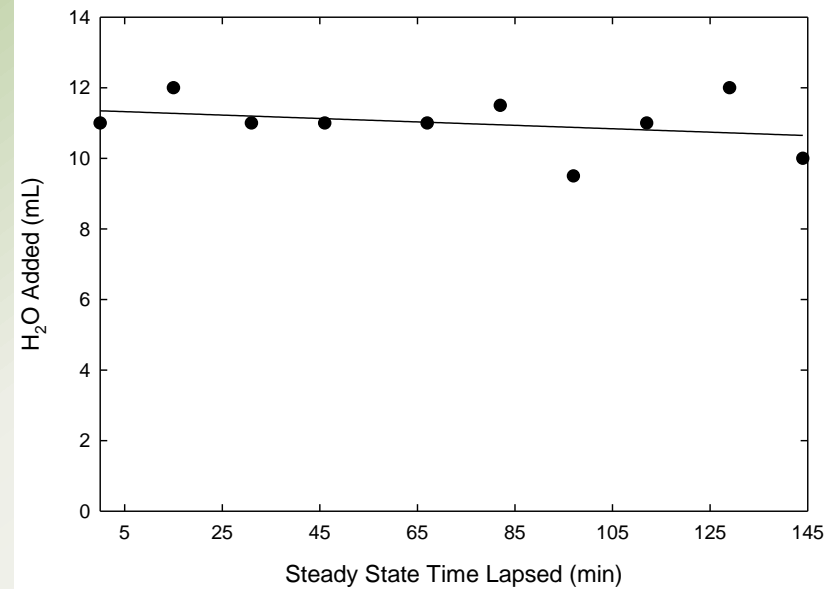
Approximately 94 days until cores were saturated

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$$h_{\text{sat}} = 6.7 \times 10^{-8}$$



$$h_{\text{sat}} = 4.0 \times 10^{-8}$$

Achieved comparable  $h_{\text{sat}}$  in field as compared to lab. Higher level of compaction with loaded trucks.

# Conclusions

- Lab findings confirmed  $h_{\text{sat}}$  results from da Rosa et al. (2013)
- Field implementation yielded comparable  $h_{\text{sat}}$  to that produced in lab
- Can create effective low permeable barrier using brown weathered sandstone



# Implications

- Isolating problematic spoil is critical of larger strategy to minimize impacts of mining (new and AML)
- Other necessary components include ...
  - ▣ Mine operations and planning
  - ▣ Construction of weep berms
  - ▣ Reforestation
  - ▣ Stream network



# Acknowledgements

- Greg Higgins at Middle Fork Development
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# Questions?



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